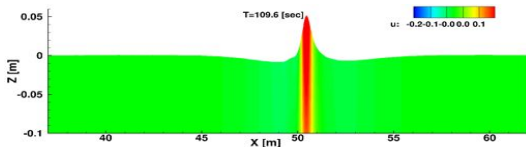


# Numerical Modelling of Deep and Shallow Water Waves with Variational Discontinuous Finite Element Methods

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## 1 Introduction

## 2 Bore Soliton Splash

## 3 Variational Space-Plus-Time Water Waves

## 4 Conclusion

## 5 Appendix

## 6 Kamiltonian

# 1. Introduction

Some hydrodynamics . . . rogue waves are anomalously high waves defined relative to a significant wave height  $H_s$ .

- Index (Khariff et al. '09, Dysthe et al. '08):

$$AI = H_{rw}/H_s > 2 \quad \text{or} \quad AI = \eta_{rw}/H_s > 1.25 \quad (1)$$

- Relevance in maritime & coastal engineering —ship design & safety offshore structures
- **Pyramidal** rogue wave (Faulkner 2001):



Fig.1. Pyramidal wave off south Japan

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Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

# Introduction

Geometric  
FEM

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Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

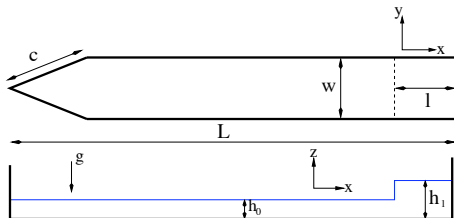
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Causes rogue waves, e.g., Khariff et al. (2009) & Faulkner (2001, 2003):

- spatial wave focussing due to refraction or wave caustics, or **wave focussing** in coastal convergences
- **crossing seas**, nearly standing waves with pyramidal waves
- emerging envelope solitons in wave train.

## 2. Bore Soliton Splash

- Water channel:  $L = 43.5 \pm 0.25\text{m}$ ,  $D = 1.20\text{m}$ ,  
 $w = 2 \pm 0.05\text{m}$



- Sluice compartment & gate, lifted with  $2.5\text{m/s}$
- V-shaped or linear convergence at other end with  $c = 2.7\text{m}$
- Start at rest with water levels  $h_0 \in [0.32, 0.47]\text{m}$  and  $h_1 \in [0.67, 1.02]\text{m}$ .

# Bore Soliton Splash

- 7+2 Cases of which 3 repeats (reproducibility):

#	$h_0$ (m) $\pm 0.01\text{m}$	$h_1$ (m) $\pm 0.01\text{m}$	$H_s$ $\pm 0.05\text{m}$	$H_{rw}$ $\pm 0.5\text{m}$	Peak #	Comments
1	0.32	0.67	-	0.6	-	bore
2	0.38	0.74	-	2.5	-	good splash
3	<u>0.41</u>	<u>0.9</u>	0.35	3.25	2 <sup>nd</sup>	thin jet cf. 6 & 8
4	0.47	1.0	0.35	1	2 <sup>nd</sup>	bore & low
5	0.41	1.02	0.40	1.5	1 <sup>st</sup>	bore & low
6	<u>0.41</u>	<u>0.9</u>	0.35	3.5	2 <sup>nd</sup>	BSS cf. 3 & 8
7	0.45	0.8	0.35	2.5	2 <sup>nd</sup>	good splash
8	<u>0.41</u>	<u>0.9</u>	0.35	3.5	2 <sup>nd</sup>	BSS & ++
9	0.43	0.9	0.45	1.8	1 <sup>st</sup>	bubble

# Intermezzo: Phenomenology Bore Soliton Splash

Geometric  
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Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Estimated wave amplitudes  $H_s \in [0.35, 0.45]$ m
- After opening sluice gates three solitary waves emerge: large, medium and small
- First highest soliton often breaks into spilling breaker
- **Variety of outcomes:** minor/major reflections, resonances between waves, smooth waves, sheets, pyramidal waves
- $H_{rw} \in [0.6, 3.5]$ m.

# Intermezzo: Bore-Soliton-Splash

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

Highest Cases 3, 6 & 8:

- $H_s = 0.35\text{m}$  &  $H_{rw} = [3.25, 3.5, 3.5]\text{m}$

- *bore soliton splash*

Wout Zweers youtube channel:

<https://www.youtube.com/watch?v=YSXsXNX4zW0>

- Truly rogish:

$$Al = \frac{H_{rw}}{H_s} = \frac{3.5}{0.35} \approx 10.$$



# Model Rogues Waves such as Bore-Soliton-Splash

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- Goal: **simulate** rogue waves **accurately**.

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

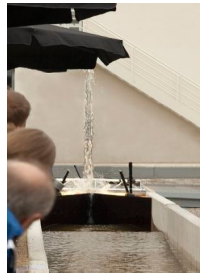
a)



b)



c)



# 3. Space-plus-Time Finite Element Water Waves

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Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

Key geometric issues:

- in the **spatial discretization** of Miles' variational principle for dispersive nonlinear water waves, and
- in the **temporal discretization** of the **non-autonomous** spatially discrete variational principle.

Verification and validation against measurements of **nonlinear waves driven by a piston wave maker**.

# Space-plus-Time Finite Element Water Waves

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Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

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Consider the (2D) potential flow water wave problem:

- gravity as restoring force with acceleration  $g$
- velocity  $\mathbf{u} = (u, w)^T = \nabla\phi$  with velocity potential  $\phi = \phi(x, z, t)$
- domain  $\Omega(t)$  with bottom  $S_B$ , wall  $S_L : x = L$  and piston wave maker at  $S_W : x = R(t)$ :

$$\Omega(t) : R(t) < x < L \quad \text{and} \quad -H(x) < z < \eta(x, t) \quad (2)$$

- free surface variables  $\eta(x, t)$  &  $\phi_s = \phi(x, z = \eta(x, t), t)$
- kinematic **single-valued** free surface  $z = \eta(x, t)$ :

$$\partial_t \eta + \partial_x \phi \partial_x \eta = \partial_z \phi \quad \text{at} \quad z = \eta(x, t) \quad (3)$$

- dynamic free surface condition: continuity of pressure.

# Miles' Variational Principle

- Miles 1977 (see also Cotter & B. 2010):

$$\begin{aligned} 0 &= \delta \int_0^T \mathcal{L}[\phi, \phi_s, \eta, t] dt \\ &= \delta \int_0^T \phi_s \partial_t \eta - \mathcal{H}[\phi, \phi_s, \eta, t] dt \\ &= \delta \int_0^T \int_{R(t)}^L \phi_s \partial_t \eta - \frac{1}{2} g \eta^2 \\ &\quad - \int_{-H(x)}^{\eta(x,t)} \frac{1}{2} |\nabla \phi|^2 dz dx - \int_{-H_w}^{\eta_w} \frac{dR}{dt} \phi_w dz dt \end{aligned}$$

- piston wave-maker  $R(t)$  with  $\phi_w \equiv \phi(R(t), z, t)$ ,  
 $H_w = H(R(t))$ ,  $\eta_w = \eta(R(t), t)$
- non-autonomous due to piston wave-maker
- canonical Hamiltonian system.

# Miles' Variational Principle

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Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

Variations yield **dynamic/kinematic conditions** and **Laplace's equation**, BC's:

$$\delta\eta(x, t) : \partial_t\phi_s + \frac{1}{2}(\partial_x\phi)^2 + g\eta - \frac{1}{2}(\partial_z\phi)_s^2(1 + (\partial_x\eta)^2) = 0$$

$$\delta\phi_s(x, t) : \partial_t\eta + \partial_x\phi_s\partial_x\eta - (\partial_z\phi)_s(1 + (\partial_x\eta)^2) = 0$$

$$\delta\phi(x, z, t) : \nabla^2\phi = 0$$

$$\delta\phi_w : dR/dt - (\partial_x\phi)_w = 0$$

$$\delta\phi_{B,L} : \mathbf{n} \cdot \nabla\phi = 0$$

# Geometric Wave Modeling: Space FEM

Geometric  
FEM

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Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

FEM formulation of Miles' variational principle.

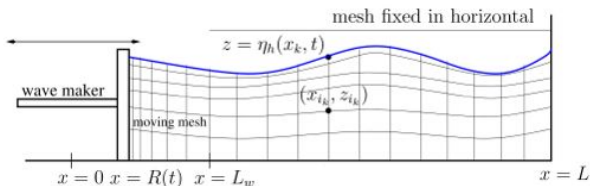
- FEM test/basis functions  $\tilde{\varphi}_j(x, z, t), \varphi_k(x, t)$  with  $i, j$  in  $\Omega$
- Indices  $k, l, r$  at free surface,  $i', j'$  in interior &  $m, \tilde{m}$  at wave maker
- Substitute finite element expansions directly into VP:

$$\phi_h(x, z, t) = \phi_j(t)\tilde{\varphi}_j(x, z, t)$$

$$\phi_{sh}(x, t) = \phi_l(t)\varphi_l(x, t)$$

$$\eta_h(x, t) = \eta_k(t)\varphi_k(x, t)$$

# Space FEM: Key Issues



- Moving mesh:
- **Issue 1:** realize that variations of interior nodes of mesh are (dynamically) coupled to variations of free surface nodes.
- **Issue 2:** find robust (variational) time integrators for (non-)autonomous system.
- Otherwise: nonlinearly unstable discretization (cf. DGFEM in 2007).

# Geometric Wave Modeling: Space FEM

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- The resulting **spatially discrete** non-autonomous VP:

$$\begin{aligned} 0 &= \delta \int_0^T L[\phi, \tilde{\varphi}, \eta, t] dt \\ 0 &= \delta \int_0^T M_{kl} \phi_k \frac{d\eta_l}{dt} - H[\phi, \tilde{\varphi}, \eta, t] dt \\ &= \delta \int_0^T M_{kl} \phi_k \frac{d\eta_l}{dt} - D_{kl} \phi_k \eta_l - \\ &\quad - \frac{1}{2} g M_{kl} \eta_k \eta_l - \frac{1}{2} A_{ij} \phi_i \phi_j - W_m \phi_m dt. \end{aligned}$$

- $M_{kl}, D_{kl}, A_{ij}, W_m$  depend on  $\{\eta_k(t), t\}$ : mesh and wave maker movements.



# Geometric Wave Modeling: Space FEM

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- The matrices and vectors depend on  $\{\eta_k(t), t\}$  as follows:

$$M_{kl}(t) = \int_{R(t)}^L \varphi_k \varphi_l dx$$

$$D_{kl}(t) = - \int_{R(t)}^L \frac{\partial \varphi_k}{\partial t} \varphi_l dx,$$

$$A_{ij}(\eta, t) = \int_{\Omega_h} (\nabla \tilde{\varphi}_i \cdot \nabla \tilde{\varphi}_j) dx dz$$

$$W_m(\eta_1, t) = \int_{-H_w}^{\eta_1} \frac{dR}{dt} \tilde{\varphi}_m|_{x=R(t)} dz,$$

- due to wave maker via  $R(t)$  & mesh movement via  $\eta(x, t)$ .

# Geometric Wave Modeling: Space FEM

- **Issue 1:** variation yields

$$\begin{aligned}\delta\phi_k &: M_{kl} \frac{d\eta_l}{dt} - D_{kl}\eta_l - A_{ik}\phi_i - W_1\delta_{1k} = 0 \\ \delta\eta_l &: \frac{d(M_{kl}\phi_k)}{dt} + D_{kl}\phi_k + M_{kl}\eta_l + \frac{1}{2} \frac{\partial A_{ij}}{\partial \eta_l} \phi_i \phi_j \\ &\quad + \frac{\partial W_m}{\partial \eta_1} \delta_{1l} \phi_m = 0 \\ \delta\phi_{j'} &: A_{ij'}\phi_i + W_{m'}\delta_{m'j'} = 0\end{aligned}$$

- Hence, we can eliminate interior degree of freedom:

$$\begin{aligned}A_{i'j'}\phi_{i'} &= -A_{lj'}\phi_l + W_{m'}\delta_{m'j'} \implies \\ \phi_{i'} &= -A_{lj'}^{-1}A_{j'i'}\phi_l - W_{m'}^{-1}A_{m'i'}^{-1}.\end{aligned}$$

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

# Geometric Wave Modeling: Space FEM

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Eliminate  $\phi_{j'}$ : **spatially discrete** VP at free surface:

$$0 = \delta \int_0^T L[\phi, \eta, t] dt$$

$$0 = \delta \int_0^T M_{kl} \phi_k \frac{d\eta_l}{dt} - H[\phi, \eta, t] dt$$

$$= \delta \int_0^T M_{kl} \phi_k \frac{d\eta_l}{dt} - D_{kl} \phi_k \eta_l -$$

$$-\frac{1}{2} g \eta_k \eta_l - \frac{1}{2} B_{kl} \phi_k \phi_l - C_l \phi_l - F_w dt.$$

- Cf. discrete **Boundary Element Method**
- Function  $F_w(t) = -\frac{1}{2} W_{\tilde{m}'} A_{\tilde{m}'m'}^{-1} W_{m'}$  & Schur complement

$$B_{kl}(\eta, t) = (A_{kl} - A_{ki'} A_{i'j'}^{-1} A_{j'l})$$

$$C_l(\eta, t) = W_1 \delta_{1l} - A_{lj'} A_{j'm'}^{-1} W_{m'}.$$

# Geometric Wave Modeling: Time FEM

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Substitute a discontinuous Galerkin finite element expansion into the VP in each time slab  $[t_n, t_{n+1}]$ :

$$\eta_l = \eta_l^{n,+} \left( \frac{t_{n+1}-t}{\Delta t_n} \right) + \eta_l^{n+1,-} \left( \frac{t-t_n}{\Delta t_n} \right)$$
$$\phi_k = \phi_k^{n+\frac{1}{2}} \frac{2(t-t_n)}{\Delta t_n} + \phi_k^{n,+} \left( \frac{t_n+t_{n+1}-2t}{\Delta t_n} \right).$$

- Define the delta function due to  $M_{kl}\phi_k d\eta_l/dt$ -term by splitting node  $n$  in a narrow element with  $C^0$ -connection, and calculating its contribution in the limit of zero width:

$$p = M_{kl}\phi_k = p_L + (p_R - p_L)(4\tau - 3\tau^2)$$

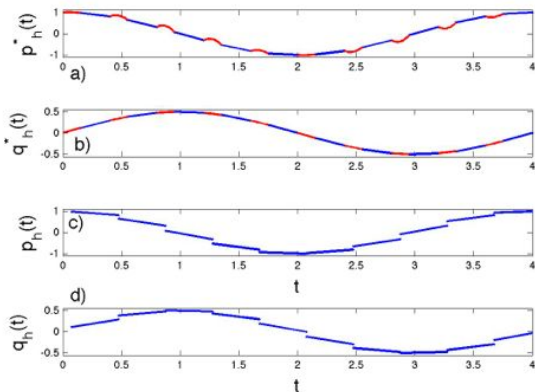
$$q = \eta_l = q_L + (q_R - q_L)\tau$$

$$\int_0^1 p \frac{dq}{d\tau} d\tau = p_R(q_R - q_L) = M_{kl}^{n+1,+} \phi_k^{n+1,+} (\eta_l^{n+1,+} - \eta_l^{n+1,-}).$$

# Limit Continuous to Discontinuous Galerkin FEM

- The integral over  $p_h dq_h/dt$  over an even element becomes

$$\int_0^1 p_h \frac{dq_h}{d\tau} d\tau = p_R^*(q_R^* - q_L^*). \quad (4)$$



Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

# Geometric Wave Modeling: Time FEM

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- **Issue 2:** algebraic VP with “extended Hamiltonian”  $H$ :

$$\begin{aligned} 0 &= \delta \sum_{n=0}^N L[\phi^{n,+}, \phi^{n+1/2}, \eta^{n,+}, \eta^{n+1,-}] dt \\ &= \delta \sum_{n=0}^N M_{kl}^{n+1/2} \phi_k^{n+1/2} (\eta_l^{n+1,-} - \eta_l^{n,+}) \\ &\quad - \frac{\Delta t}{2} (H^{n+1/2}[\phi^{n+1/2}, \eta^{n,+}] + H^{n+1/2}[\phi^{n+1/2}, \eta^{n+1,-}]) \\ &\quad + \delta \sum_{n=-1}^N M_{kl}^{n+1,+} \phi_k^{n+1,+} (\eta_l^{n+1,+} - \eta_l^{n+1,-}) \end{aligned}$$

# Intermezzo: Time FEM

- Variations (evaluation  $\dagger = n + 1/2$ ):

$$\delta\phi_k^{n+1,+} : \eta_l^{n+1,+} = \eta_l^{n+1,-} \quad \text{continuous!}$$

$$\delta\eta_l^{n,+} : M_{kl}^{n+1/2} \phi_k^{n+1/2} = M_{kl}^n \phi_k^{n,+} \\ - \frac{1}{2} \Delta t \frac{\partial H^{n+1/2}[\phi^{n+1/2}, \eta^{n,+}]}{\partial \eta_l^{n,+}}$$

$$\delta\phi_k^{n+1/2} : M_{kl}^{n+1/2} \eta_l^{n+1,-} = M_{kl}^{n+1/2} \eta_l^{n,+} \\ + \frac{1}{2} \Delta t \left( \frac{\partial H^\dagger[\phi^{n+1/2}, \eta^{n,+}]}{\partial \phi_k^{n+1/2}} + \frac{\partial H^\dagger[\phi^{n+1/2}, \eta^{n+1,-}]}{\partial \phi_k^{n+1/2}} \right)$$

$$\delta\eta_l^{n+1,-} : M_{kl}^{n+1,+} \phi_k^{n+1,+} = M_{kl}^{n+1/2} \phi_k^{n+1/2} \\ - \frac{1}{2} \Delta t \frac{\partial H^{n+1/2}[\phi^{n+1/2}, \eta^{n+1,-}]}{\partial \eta_l^{n+1,-}}$$

# Geometric Wave Modeling: Unfolding

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Reduces to 2nd-order symplectic Störmer-Verlet time integrator in the autonomous case
- Reduces to 2nd-order symplectic Störmer-Verlet time integrator “Kamiltonian” non- autonomous case
- “Unfold” the kinetic energy term again to avoid direct inversion of the matrix  $A_{i'j'}$
- This defines the nature of the time discretization of  $\phi_{i'}$  in the interior
- Use Newton iteration and Petsc linear algebra routines.



# Intermezzo: Unfolding

- “Unfold” the kinetic energy term again:

$$\sum_{n=0}^N \frac{1}{2} \Delta t^n (K^\dagger(\tilde{\phi}^{n,+}, \phi^\dagger, \eta^{n,+}) + K^\dagger(\tilde{\phi}^{n+1,-}, \phi^\dagger, \eta^{n+1,-})) \equiv$$

$$\sum_{n=0}^N \frac{\Delta t^n}{4} (B_{kl}^\dagger(\eta^{n,+}) + B_{kl}^\dagger(\eta^{n+1,-})) \phi_k^{n+1/2} \phi_l^\dagger =$$

$$\sum_{n=0}^N \frac{\Delta t^n}{4} (A_{kl}^\dagger(\eta^{n,+}) \phi_k^\dagger \phi_l^\dagger + A_{kl}^\dagger(\eta^{n+1,-}) \phi_k^\dagger \phi_l^\dagger$$

$$+ A_{kj'}^\dagger(\eta^{n,+}) \phi_k^\dagger \phi_{j'}^{n,+} + A_{kj'}^\dagger(\eta^{n+1,-}) \phi_k^\dagger \phi_{j'}^{n+1,-}$$

$$+ A_{i'l}^\dagger(\eta^{n,+}) \phi_{i'}^{n,+} \phi_l^\dagger + A_{i'l}^\dagger(\eta^{n+1,-}) \phi_{i'}^{n+1,-} \phi_l^\dagger$$

$$+ A_{i'j'}^\dagger(\eta^{n,+}) \phi_{i'}^{n,+} \phi_{j'}^{n,+} + A_{i'j'}^\dagger(\eta^{n+1,-}) \phi_{i'}^{n+1,-} \phi_{j'}^{n+1,-})$$

# Geometric Wave Modeling: Validation

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

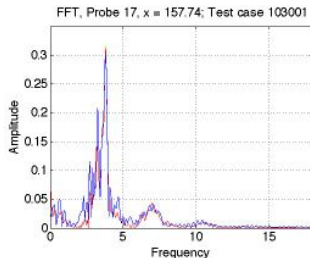
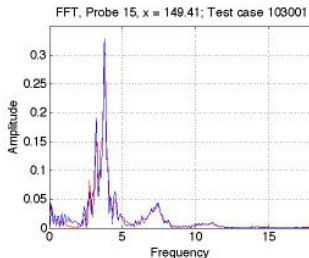
Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- *Driven wave focusing* in MARIN's wave tank  
[http://www1.maths.leeds.ac.uk/~obokhove/202002\\_zoom\\_splash\\_2.avi](http://www1.maths.leeds.ac.uk/~obokhove/202002_zoom_splash_2.avi)
- Entire *wave tank* MARIN with false vertical wall instead of *beach* (Kristina, B. Van Groesen 2014 run-up tsunami's).
- Comparison with measured data MARIN is good:



## 4. Conclusion

- Posed simulation challenges: rogue waves.
- **Key issues** in variational nonlinear water wave modelling.
- **Discontinuous Galerkin variational time approach generalizes** to new pseudo-symplectic integrators.
- All extends to 3D & more general mesh movement.
- Extend numerics to **hybrid geometric model** with potential flow limit & depth-averaged shallow water limit (Cotter & Bokhove 2010, Gagarina et al. 2013).
- Extend numerics to **mixture theoretic 2-phase model** with intermittent breaking waves, & geometric potential flow model as limit (Bokhove 2014).
- ... **break through** experiment.
- Funding: NWO, STW & SFFF.

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

# Bore Soliton Splash & Tohoku Tsunami

Geometric  
FEM

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Bokhove

Introduction

Bore Soliton  
Splash

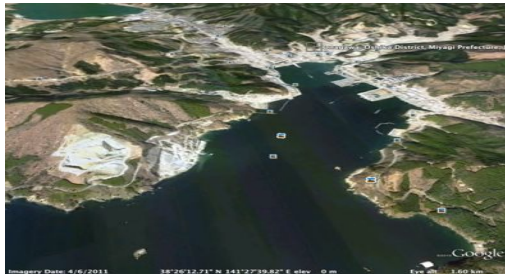
Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- “Critical run-up factors and impact ... Tohoku Tsunami” by Lekkas et al. 2011.
- Vertical run-up Tohoku tsunami highest in **Onagawa Bay**: 42m for a rough estimate of 7.5m high incoming waves.
- Ratio run-up/wave height:  $AI \approx 5.5$  (**shallow water rogue waves** Nikolkina & Didenkulova 2011).
- Recall BSS/incoming wave height is  $AI \approx 10$ .



# References

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# Kamiltonian: Time FEM

- Reformulate **non-autonomous** Hamiltonian system; change  $t = \tilde{t} \rightarrow \tau$  & then make  $\tau = \tau(t)$ :

$$0 = \delta \int_0^T M_{kl}(\tau) \phi_k \frac{d\eta_l}{d\tau} - H[\phi, \eta, \tau] d\tau \implies$$

$$0 = \delta \int_0^T M_{kl}(\tau) \phi_k \frac{d\eta_l}{dt} + p \frac{d\tau}{dt} - H[\phi, \eta, \tau] - p dt$$

- Dynamics in new conjugate variables  $\{M\phi, \eta\}, \{p, \tau\}$  with autonomous **Kamiltonian**  $K(\phi, \eta, \tau, p) = H(\phi, \eta, \tau) + p$ :

$$\delta p : d\tau/dt = \partial K/\partial p = 1, \quad \delta \tau : \dots$$

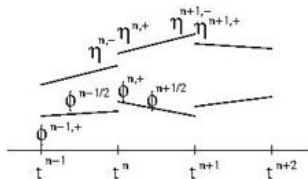
$$\delta \phi_k : M_{kl} d\eta_l/dt = \partial H/\partial \phi_k$$

$$\delta \eta_l : d(M_{kl} \phi_k)/dt = -\partial H/\partial \eta_l$$

- Equation for **p decoupled** from rest.

# Intermezzo: Time FEM

- Introduce **time slabs** & expand variables discontinuously:



- Use in VP with **jump terms** at time nodes:

$$0 = \delta \sum_{n=0}^N \int_{t^n}^{t^{n+1}} M_{kl}(\tau) \phi_k \frac{d\eta_l}{dt} + p \frac{d\tau}{dt} - H[\phi, \eta, \tau] - p dt +$$

$$\sum_{n=-1}^N M_{kl}(\tau^{n+1,+}) (\eta_l^{n+1,+} - \eta_l^{n+1,-}) + p^{n+1,+} (\tau^{n+1,+} - \tau^{n+1,-})$$

# Intermezzo: Time FEM

- Use **quadrature** to get algebraic VP:

$$\begin{aligned} 0 = & \delta \sum_{n=0}^N M_{kl}^{n+1/2} \phi_k^{n+1/2} (\eta_l^{n+1,-} - \eta_l^{n,+}) \\ & + p^{n+1/2} (\tau^{n+1,-} - \tau^{n,+}) \\ & - \frac{\Delta t}{2} (H[\phi^{n+1/2}, \boldsymbol{\eta}^{n,+}, \tau^*] + H[\phi^{n+1/2}, \boldsymbol{\eta}^{n+1,-}, \tau^{**}]) \\ & - \Delta t p^{n+1/2} + \delta \sum_{n=-1}^N (M_{kl}^{n+1,+} \phi_k^{n+1,+} (\eta_l^{n+1,+} - \eta_l^{n+1,-}) \\ & + p^{n+1,+} (\tau^{n+1,+} - \tau^{n+1,-})) \end{aligned}$$

- Time  $\tau$  becomes continuous:  $\delta p^{n+1,+} : \tau^{n+1,+} = \tau^{n+1,-}$ !
- Previously used:  $\tau^* = \tau^{**} = \tau^{n+1/2}$ .  
Alternative:  $\tau^* = \tau^{n,+}, \tau^{**} = \tau^{n+1,-}$ .



# Time DGFEM: Stormer-Verlet

- Discrete Lagrangian ( $\gamma = 0$ ):

$$\begin{aligned} L_h(p_h, q_h) &= \sum_{n=-1}^N (q^{n+1} + q^n - 2q^{n+1/2}) p_r^{n+1} \\ &+ \sum_{n=0}^{N-1} (p_l^{n+1} + p_r^{n+1})(q^{n+1/2} - q^n) \\ &- \frac{\Delta t_n}{2} (H(p_l^{n+1}, q^{n+1/2}) + H(p_r^{n+1}, q^{n+1/2})) \end{aligned}$$

- Stormer-Verlet with  $p_l^{n+1} = p_r^n$  continuous &  $q$  remains DG:

$$\delta p_l^{n+1} : q^{n+1/2} = q^n + \Delta t p_l^{n+1} / 2$$

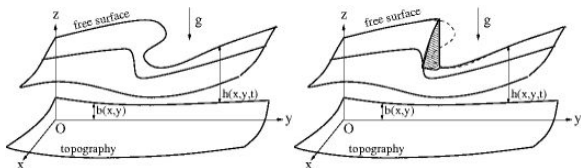
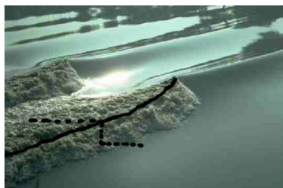
$$\delta q^{n+1/2} : p_r^{n+1} = p_l^{n+1} - \frac{\Delta t}{2} ((q^{n+1/2})^3 + (q^{n+1/2})^3)$$

$$\delta p_r^{n+1} : q^{n+1} = q^{n+1/2} + \Delta t p_r^{n+1} / 2$$

# Bores in Boussinesq Models

Derived a **new water wave model** (Cotter & B. 2010, Gagarina et al. 2013c):

- full water wave dispersion & potential flow as limit
- depth-averaged shallow water equations as other limit
- bore relations (if any) derived variationally (Clebsch):



# New Water Wave Model

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Dynamics of surface variables  $\mathbf{u}^*(x, y, t)$ ,  $h(x, y, t)$ :

$$\partial_t h + \nabla \cdot (h\bar{\mathbf{u}}) = 0 \quad (5a)$$

$$\partial_t \mathbf{u}^* + \nabla B + qh\bar{\mathbf{u}}^\perp = 0, \quad (5b)$$

where  $h\bar{\mathbf{u}} = h\mathbf{u}^* + \int_b^{b+h} \nabla_H \varphi dz$ , PV  $q = (\partial_x v^* - \partial_y u^*)/h$   
&  $B = \frac{1}{2}|\mathbf{u}^*|^2 + g(h+b) - \frac{1}{2} \frac{((\partial_z \varphi)_s^2 (1 + |\nabla_H(h+b)|^2))}{g}$

- Interior dynamics velocity potential difference  $\varphi$ :

$$\nabla^2 \varphi + \nabla \cdot \mathbf{u}^* = 0 \quad (6)$$

- At the free surface  $z = h(x, y, t) + b(x, y)$ , the potential is  $\varphi = 0$ .

# Single-Phase Mixture Theory

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Dispersive bores difficult to model (numerically)?
- Hence, consider instead **incompressible two-phase** (here air & water) system.
- Bulk density  $\rho = \rho_l + \rho_g \equiv \rho_{0l}\varphi + \rho_{0g}(1 - \varphi)$ .
- Bulk velocity  $\rho\mathbf{u} = \rho_l\mathbf{u}_l + \rho_g\mathbf{u}_g$ .
- Equations of motion with a very **simple closure** are:

$$\begin{aligned}\partial_t \rho_l + \nabla \cdot (\rho_l \mathbf{u}_l) &= 0 \\ \rho_l (\partial_t \mathbf{u}_l + \mathbf{u}_l \cdot \nabla \mathbf{u}_l) &= -\varphi \nabla p + \rho_l \mathbf{g} - \rho_l \mathbf{c}(\mathbf{u}_l - \mathbf{u}) \\ \partial_t \rho_g + \nabla \cdot (\rho_g \mathbf{u}_g) &= 0 \\ \rho_g (\partial_t \mathbf{u}_g + \mathbf{u}_g \cdot \nabla \mathbf{u}_g) &= -(1 - \varphi) \nabla p + \rho_g \mathbf{g} - \rho_g \mathbf{c}(\mathbf{u}_g - \mathbf{u}).\end{aligned}$$

# Single-Phase Mixture Equations

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Scale species **hydrostatically** in local **pancakes** of wave breaking.
- Horizontal velocity equals **bulk velocity**.
- Vertical velocity has **segregation terms**:

$$\begin{aligned}w_l - w &= -K(1 - \varphi) \quad \text{and} \\w_g - w &= K\varphi/\tilde{\rho} \quad \text{with} \quad K = g(1 - \tilde{\rho})/c. \quad (7)\end{aligned}$$

- Density ratio  $\tilde{\rho} = \rho_{0g}/\rho_{0l}$ .

# Single-Phase Mixture Equations

Geometric  
FEM

Onno  
Bokhove

Introduction

Bore Soliton  
Splash

Variational  
Space-Plus-  
Time Water  
Waves

Conclusion

Appendix

Kamiltonian

- Now add **non-hydrostatic terms** to bulk flow only in vertical momentum equation.
- Mixed phases unmix **hydrostatically**:

$$\partial_t(\rho \mathbf{u}_H) + \nabla \cdot (\rho \mathbf{u} \mathbf{u}_H + p) = 0$$

$$\partial_t(\rho w) + \nabla \cdot (\rho \mathbf{u} w) = -\partial_z p - \rho g$$

$$\partial_t \varphi + \nabla \cdot (\mathbf{u} \varphi) - \partial_z (K \varphi (1 - \varphi)) = 0$$

$$\nabla_H \cdot \mathbf{u}_H + \partial_z (w + K \varphi (1 - \varphi) (1 - \tilde{\rho}) / \tilde{\rho}) = 0$$

$$\rho = \rho_{0g}(1 - \varphi) + \rho_{0l}\varphi$$

$$K = g(1 - \tilde{\rho})/c \quad \text{with} \quad \tilde{\rho} = \rho_{0g}/\rho_{0l}.$$

- When phases separated then **potential-flow limit** is enclosed.